


SANYO Semiconductors

DATA SHEET

An ON Semiconductor Company

LV5027M — Bi-CMOS IC LED Driver IC

Overview

LV5027M is a High Voltage LED drive controller which drives LED current up to 3A with external MOSFET.

LV5027M is realized very simple LED circuits with a few external parts.

Functions

- High Voltage LED Controller
- Low noise switching system
 - 5 stages skip mode Frequency
 - Soft driving
- Built-in Reference voltage circuit (internal 0.605V)
- Built-in circuit of detection of overvoltage of CS pin.
- Short Protection Circuit

Specifications

Maximum Ratings at Ta = 25°C

Parameter	Symbol	Conditions	Ratings	Unit
Maximum Input voltage	V _{IN} max		-0.3 to 42	V
CS pin			-0.3 to 7	V
OUT pin	V _{OUT_abs}		-0.3 to 42	V
Allowable power dissipation	P _d max	With specified board*	1.0	W
Junction temperature	T _j max		150	°C
Operating temperature	T _{opr}		-30 to +125	°C
Storage temperature	T _{stg}		-40 to +150	°C

*Specified board: 58.0×54.0×1.6mm (glass epoxy board)

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Recommended Operating Conditions at Ta = 25°C

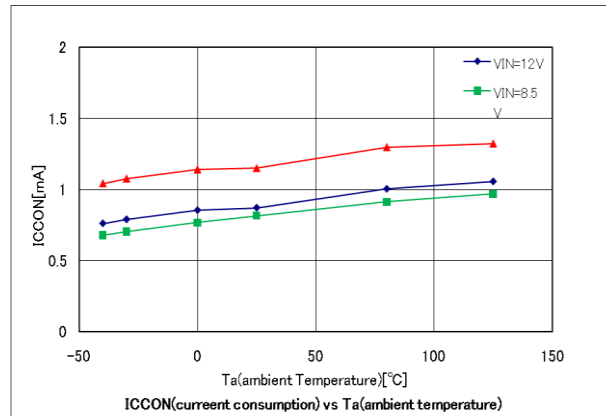
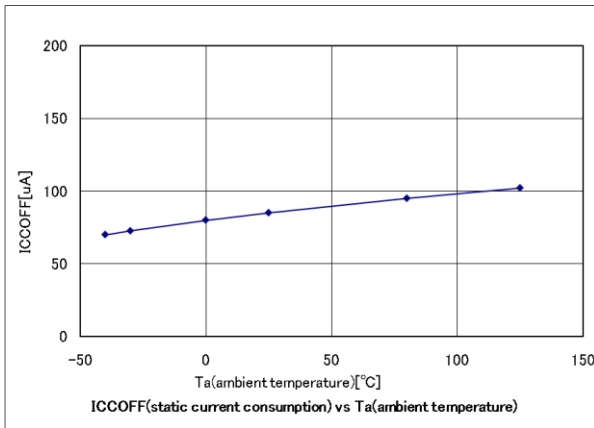
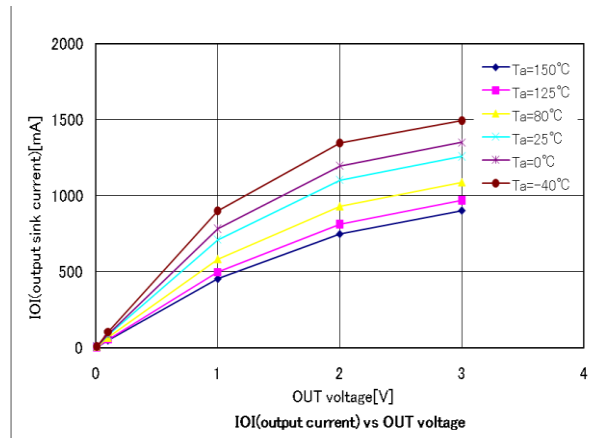
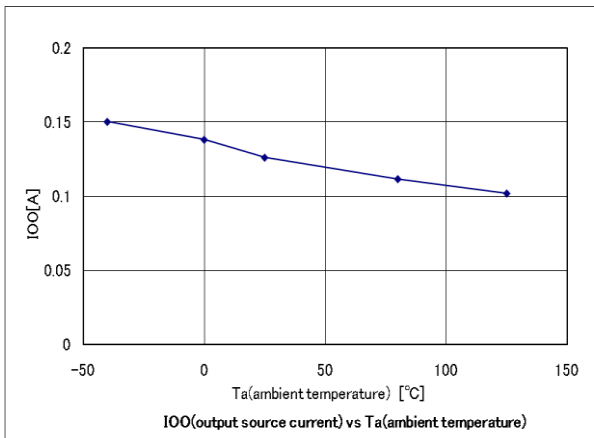
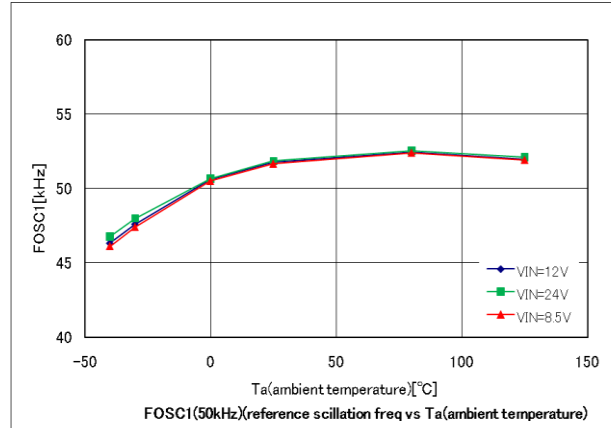
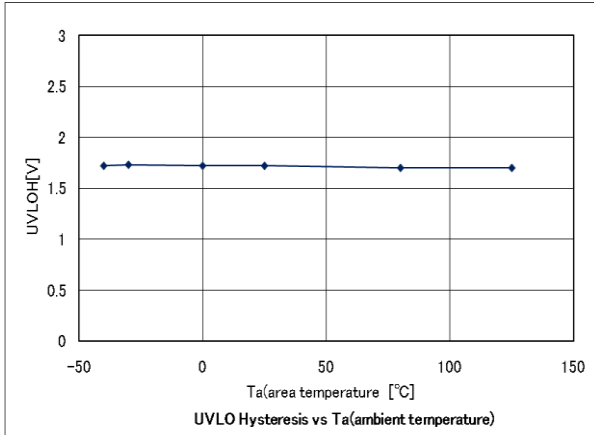
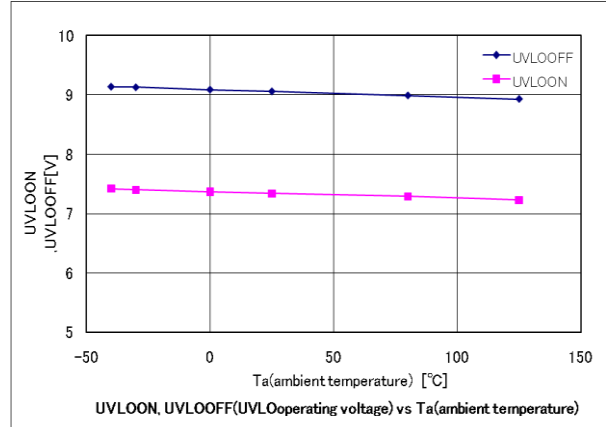
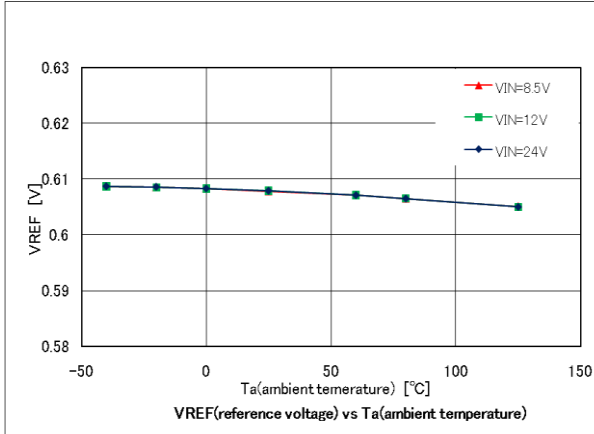
Parameter	Symbol	Conditions	Ratings	Unit
Input voltage	V _{IN}		8.5 to 24	V

Electrical Characteristics at Ta = 25°C, V_{IN} = 12V, unless otherwise specified.

Parameter	Symbol	Conditions	Ratings			Unit
			min	typ	max	
Reference Voltage block						
Built-in Reference Voltage	VREF		0.585	0.605	0.625	V
VREF VIN line regulation	VREF_LN	VIN = 8.5 to 24V		±0.5		%
Under Voltage Lockout						
Operation Start Input Voltage	UVLOON		8	9	10	V
Operation Stop Input Voltage	UVLOOFF		6.3	7.3	8.3	V
Hysteresis Voltage	UVLOH			1.7		V
Oscillation						
Frequency	FOSC		40	50	60	kHz
Maximum ON duty	MAXDuty			93		%
Comparator						
Input offset Voltage (Between CS and VREF)	VIQ_VR			1	10	mV
Input current	IIOCS			160		nA
	IIOREF			80		nA
CS pin max voltage	VOM				1	V
malfunction prevention mask time	TMSK			150		ns
Thermal protection Circuit						
Thermal shutdown temperature	TSD	*Design guarantee		165		°C
Thermal shutdown hysteresis	ΔTSD	*Design guarantee		30		°C
Drive Circuit						
OUT sink current	IOI		500	1000		mA
OUT source current	IOO			120		mA
Minimum On time	TMIN			200	300	ns
VIN current						
UVLO mode VIN current	ICCOFF	VIN<UVLOON		80	120	μA
Normal mode VIN current	ICCON	VIN>UVLOON, OUT = OPEN		0.6		mA
VIN Over Voltage Protection Circuit						
VIN over voltage protection voltage	VINOVP		24	27	30	V
VIN Current at OVP	IINOVP	VIN=30V	0.7	1.0	1.5	mA
CS terminal abnormal sensing circuit						
Abnormal sensing voltage	CSOCP			1.9		V

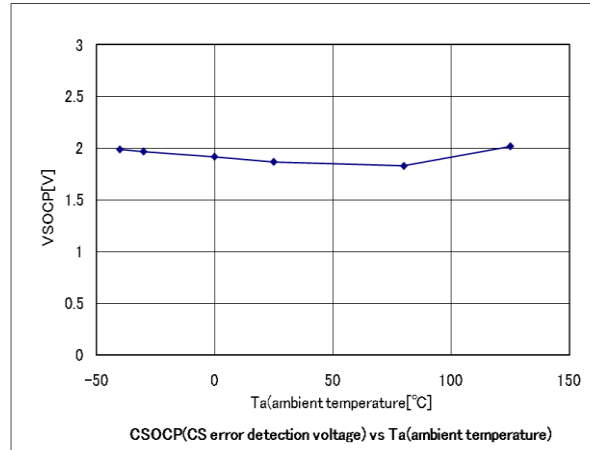
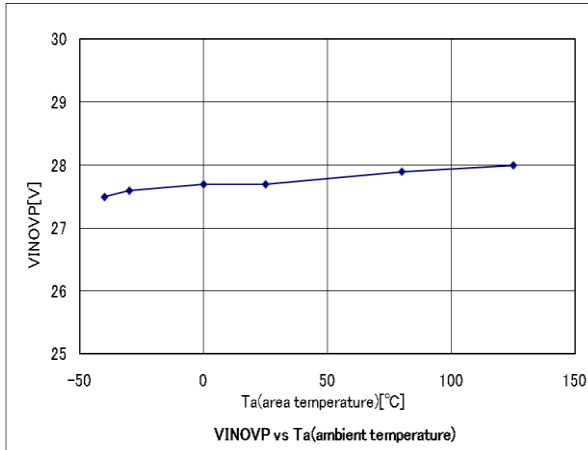
*: Design guarantee (value guaranteed by design and not tested before shipment)

TYPICAL CHARACTERISTICS



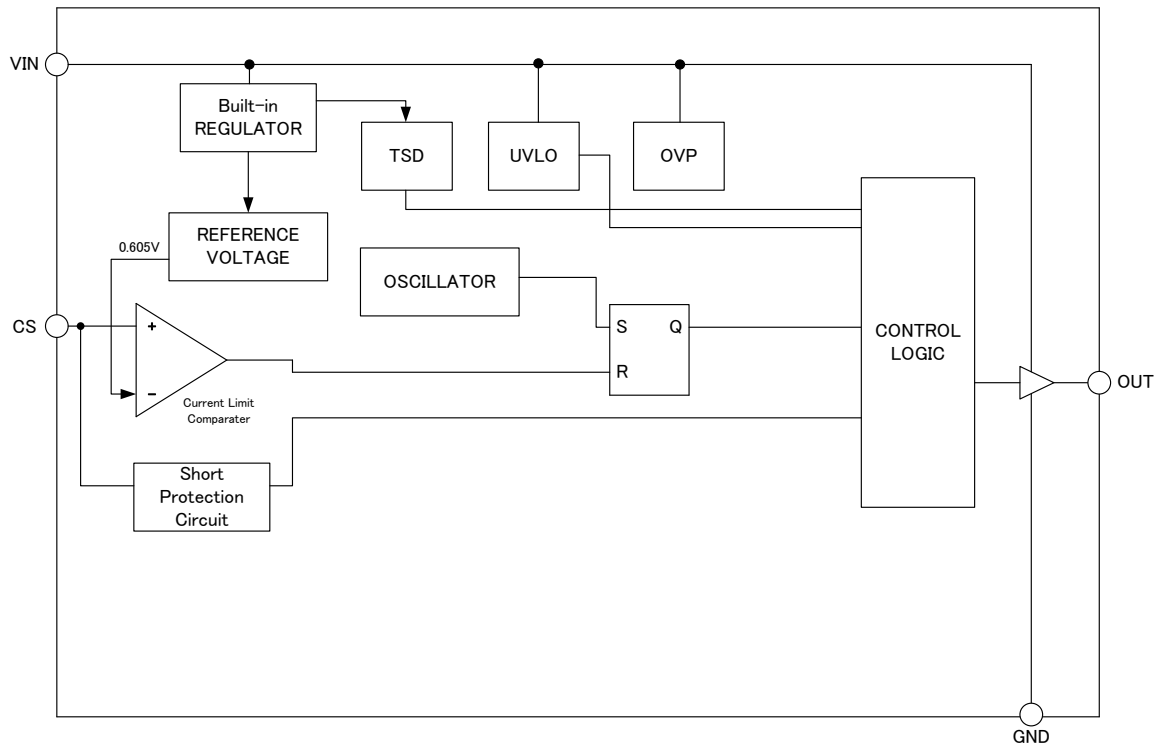
LV5027M

TYPICAL CHARACTERISTICS



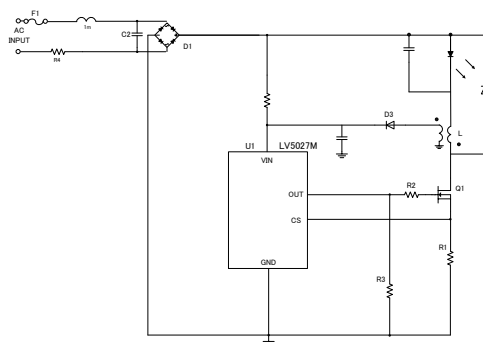
TYPICAL CHARACTERISTICS

Block Diagram

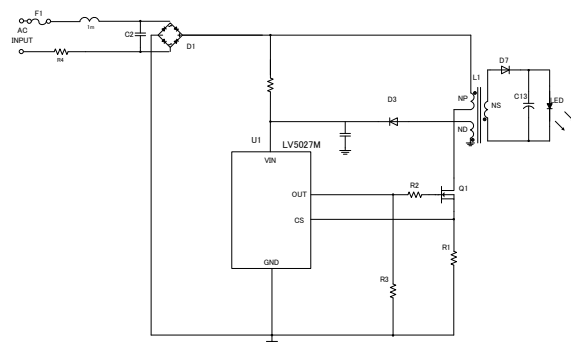


Sample Application Circuit

Non isolation



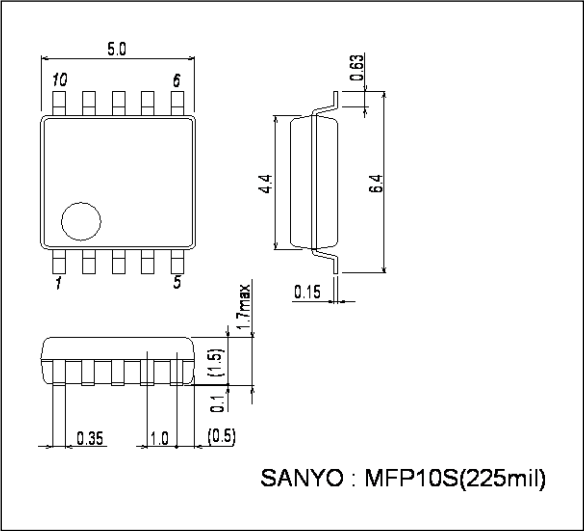
Isolation



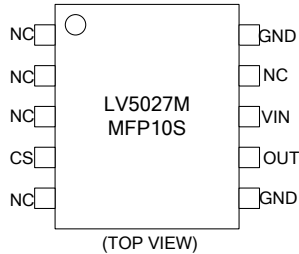
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Package Dimensions

unit: mm (typ)
3086B



Pin Assignment

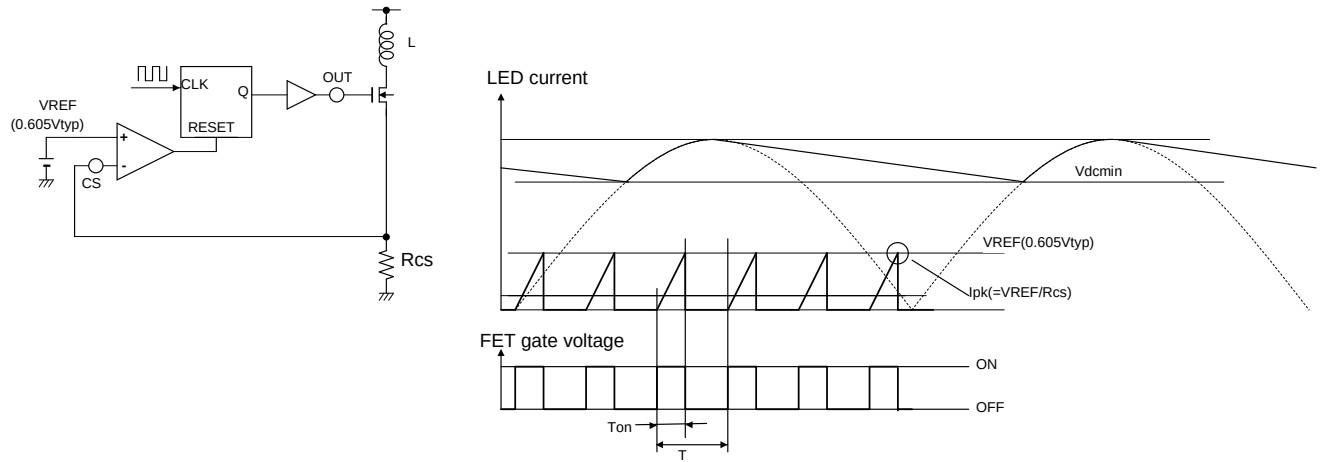


Pin Functions

pin No	Pin Name	Pin Function	Equivalent Circuit
1	NC	No connection	
2	NC	No connection	
3	NC	No connection	
4	CS	LED current sensing in. If this terminal voltage exceeds VREF, external FET is OFF. And if the voltage of the terminal exceeds 1.9V, LV5027M turns to latch-off mode.	
5	NC	No connection	
6	GND	GND pin.	
7	OUT	Driving the external FET Gate Pin.	
8	VIN	Power supply pin. Operation : $V_{IN} > UVLOON$ Stop : $V_{IN} < UVLOFF$ Switching Stop : $V_{IN} > V_{INOVP}$	
9	NC	No connection	
10	GND	GND pin.	

Relation ship between VREF and CS pin voltage

The output current value is the average of the current value that flows during one cycle. The current value that flows into coil is a triangular wave shown in the figure below. Make sure to set I_{pk} so that (average of current value at one cycle) is equal to (LED current value). I_{pk} is set by the relationship between V_{REF} (internal reference voltage) voltage and R_{cs} voltage.



$$I_{pk} = \frac{V_{REF}}{R_{cs}}$$

I_{pk} : peak inductor current

V_{IN} : AC power-supply voltage (minimum value)

V_{REF} : Built-in reference voltage (0.605V)

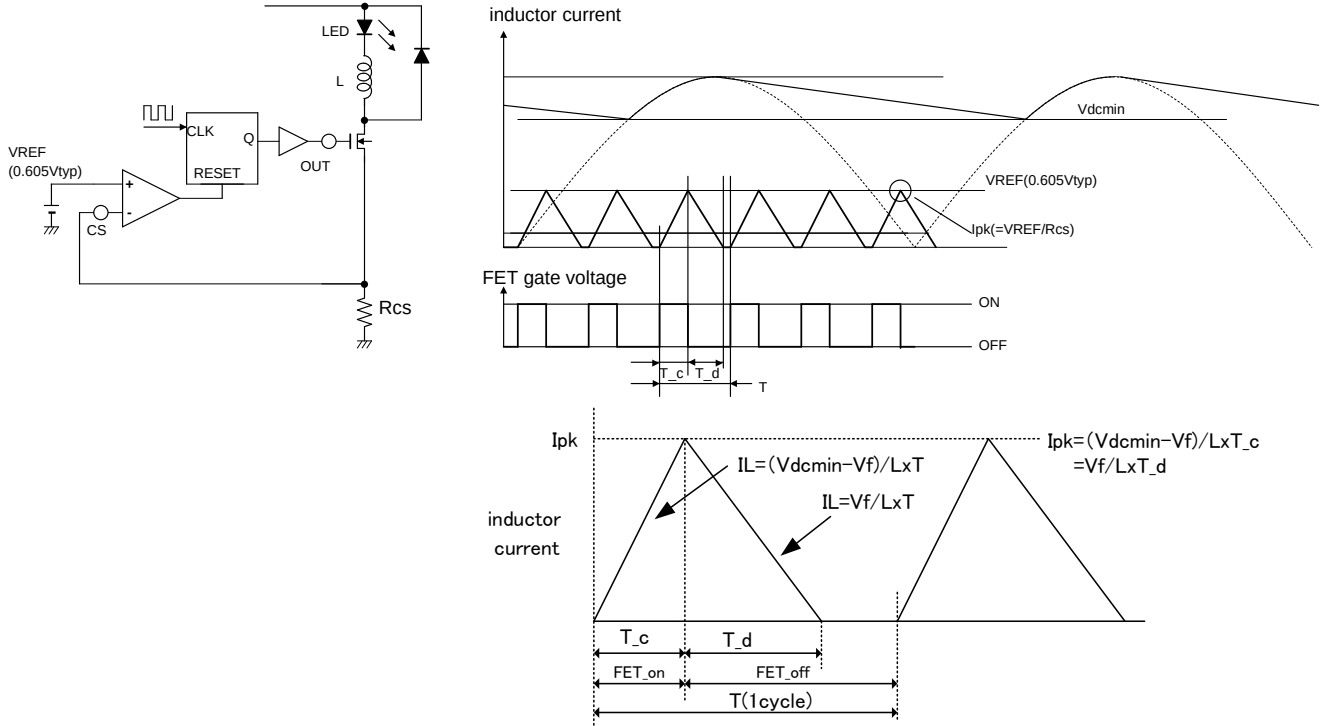
R_{cs} : External sense resistor

LED current and inductance setting

It is available to use both no-isolation and isolation applications.

(For non-isolation application)

The output current value is the average of the inductor current value that flows during one cycle. The current value that flows into inductor is a triangular wave shown in the figure below. Make sure to set I_{pk} so that (average of inductor current value at one cycle) is equal to (LED current value).



Given that the period when current flows into coil is

$$DutyI = \frac{T_c + T_d}{T}$$

$$I_{pk} \times \frac{1}{2} \times (DutyI \times T) / T = I_{LED}$$

$$I_{pk} = \frac{2 \times I_{LED}}{DutyI} \quad (1) \quad \text{since} \quad I_{pk} = \frac{V_{REF}}{R_{cs}}$$

$$R_{cs} = \frac{V_{FET}}{I_{pk}} = \frac{DutyI \times V_{REF}}{2 I_{LED}} \quad (2)$$

I_{pk} : peak inductor current
 V_f : LED forward voltage drop
 V_{dcmin} : AC power-supply voltage
 (Rectified minimum DC voltage)
 V_{REF} : Built-in reference voltage (0.605V)
 R_{cs} : External sense resistor

Since formula for LED current is different between on period and off period as shown above,

$$I_{pk} = \frac{V_{dcmin} - V_f}{L} \times T_c = \frac{V_f}{L} \times T_d \quad (3).$$

$$\text{Since } T_c + T_d = DutyI \times T, T_c = DutyI \times T - T_d \quad (4)$$

$$\text{Based on the result of (3) and (4), } T_d = DutyI \times T \times \frac{V_{dcmin} - V_f}{V_{dcmin}} \quad (5)$$

To obtain L from the equation (1), (3), (5),

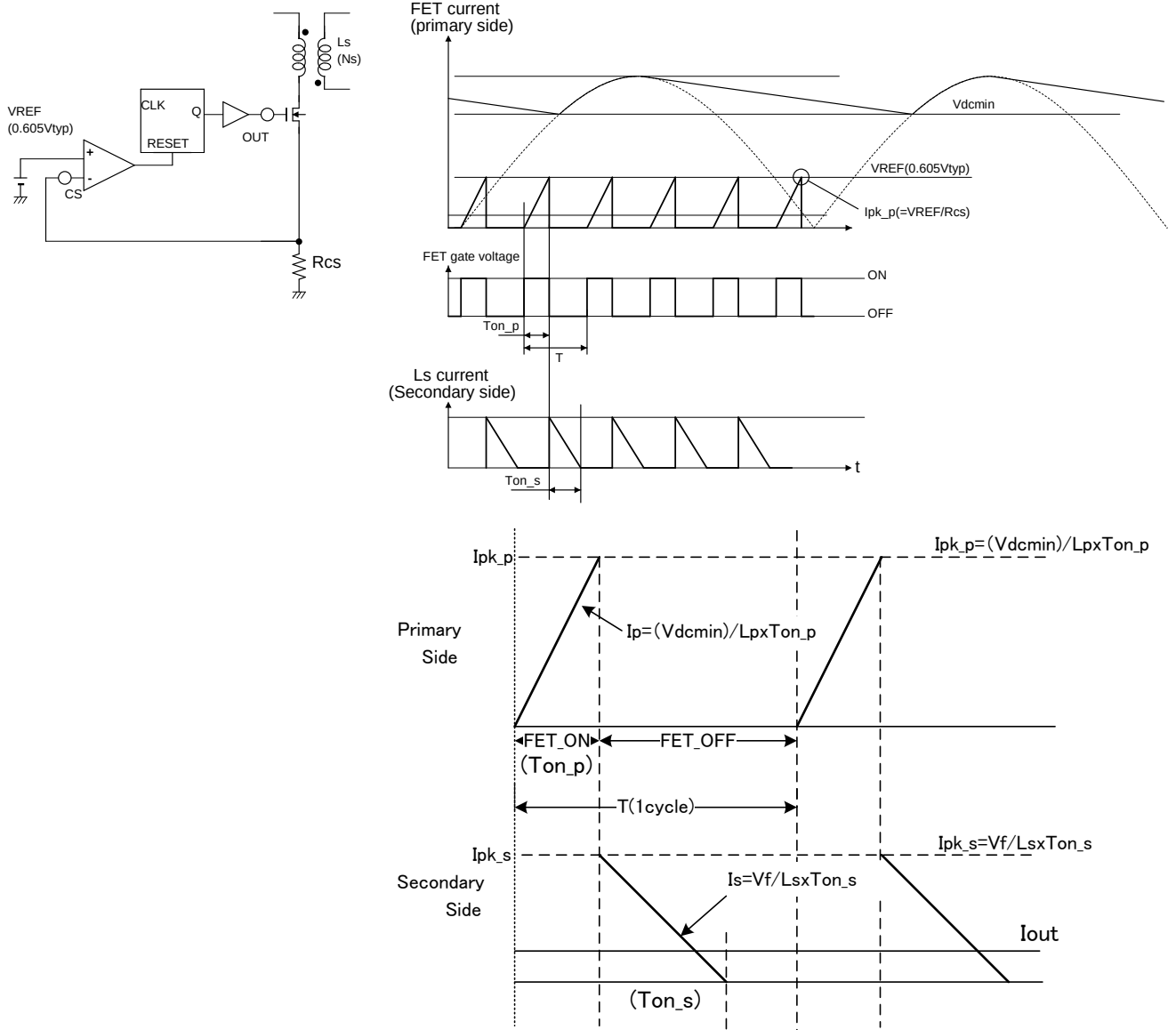
$$L = \frac{V_f \times DutyI}{2 \times I_{LED}} \times DutyI \times T \times \frac{V_{dcmin} - V_f}{V_{dcmin}} = \frac{V_f}{2 \times I_{LED}} \times \frac{1}{f_{osc}} \times \frac{V_{dcmin} - V_f}{V_{dcmin}} \times (DutyI)^2 \quad (6)$$

Since LED and inductor are connected in serial in non-isolation mode, LED current flows only when AC voltage exceed V_f .

(for Isolation application)

Using the circuit diagram below, the wave form of the current that flows to Np and Ns is as follows.

Current waveform flows to primary side and secondary



[Inductance Lp of primary side and sense resistor Rs]

If a peak current flow to transformer is represented as I_{pk_p} , the power (P_{in}) charged to the transformer on primary side can be represented as:

$$P_{in} = \frac{1}{2} \times L_p \times (I_{pk_p})^2 \times f_{osc} \quad (11)$$

$$\therefore I_{pk_p} = \frac{V_{dc\ min}}{L_p} \times T_{on_p} \quad (12)$$

$$\therefore L_p = \frac{V_{dc\ min}^2 \times T_{on_p}^2 \times f_{osc}}{2 \times P_{in}} = \frac{V_{dc\ min}^2 \times D_{on_p}^2}{2 \times P_{in} \times f_{osc}} \quad (13)$$

$$(D_{on_p} = \frac{T_{on_p}}{T} = T_{on_p} \times f_{osc})$$

To substitute the following to the formula below,

$$\therefore \eta = \frac{P_{out}}{P_{in}} \quad (14)$$

$$\therefore L_p = \frac{V_{dc\ min}^2 \times T_{on_p}^2 \times f_{osc} \times \eta}{2 \times P_{out}} = \frac{V_{dc\ min}^2 \times D_{on}^2 \times \eta}{2 \times P_{out} \times f_{osc}} \quad (15)$$

Sense resistor is obtained as follows.

$$R_s = \frac{V_{REF}}{I_{pk_p}} = \frac{V_{REF} \times L_p}{V_{dc \min} \times T_{on_p}} = \frac{V_{REF} \times L_p}{V_{dc \min} \times D_{on_p} \times T} \quad (16)$$

[Inductance L_s of secondary side]

Since output current I_{out} is the average value of current flows to transformer of secondary side

$$I_{out} = I_{pk_s} \times \frac{T_{on_s}}{T} \times \frac{1}{2} = \frac{I_{pk_s} \times D_{on_s}}{2} \quad (D_{on_s} = \frac{T_{on_s}}{T} = T_{on_s} \times f_{osc}) \quad (17)$$

$$I_{pk_s} = \frac{V_{out}}{L_s} \times T_{on_s} = \frac{V_{out}}{L_s} \times \frac{D_{on_s}}{f_{osc}} \quad (18)$$

$$L_s = \frac{V_{out} \times T \times D_{on_s}^2}{2 \times I_{out}} = \frac{V_{out} \times D_{on_s}^2}{2 \times I_{out} \times f_{osc}} = \frac{V_{out}^2 \times D_{on_s}^2}{2 \times P_{out} \times f_{osc}} \quad (19)$$

Calculation of the ratio of transformer coil on primary side and secondary side

Since ratio and inductance of transformer coil is

$$\frac{N_s}{N_p} = \frac{\sqrt{L_s}}{\sqrt{L_p}} \quad (20)$$

substituted equations (15), (19) for (20)

$$\therefore \frac{N_p}{N_s} = \frac{V_{dc \min}}{V_{out}} \times \sqrt{\eta} \times \frac{D_{on_p}}{D_{on_s}} \quad (21)$$

Calculation of transformer coil on primary side and secondary side

$$N = \frac{V_{ac} \times 10^8}{2 \times \Delta B \times A_e \times f_{osc}} \quad (22)$$

ΔB : variation range of core flux density [Gauss]

A_e : core section area [cm²]

To use Al (L value at 100T),

$$N = \sqrt{\frac{L}{Al}} \times 10^2 \quad (23)$$

L : inductance [uH]

Al : L value at 100T [uH/N²]

lg (Air gap) is obtained as follows:

$$lg = \frac{\mu_r \mu_0 N^2 A_e 10^2}{L} \quad (24)$$

μ_r : relative magnetic permeability, $\mu_r = 1$

μ_0 : vacuum magnetic permeability $\mu_0 = 4\pi \times 10^{-7}$

N : turn count [T]

A_e : core section area [m²]

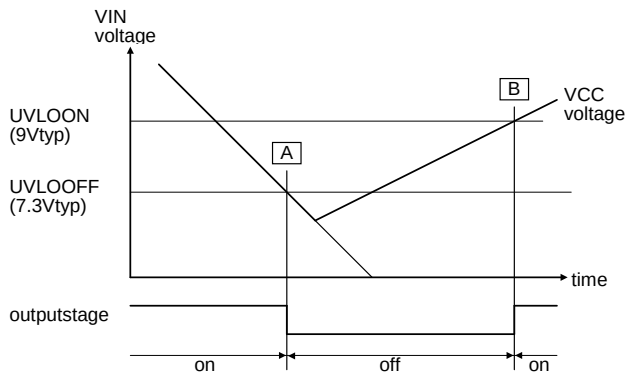
L : inductance [H]

Description of operating protection function

	tilte	outline	monitor point	note
1	UVLO	Under Voltage Lock Out	VIN voltage	
2	OC	Over Current Protection	CS voltage	equivalent FET current
3	OVP	Over Voltage Protection	VIN voltage	
4	OTP (TSD)	Over Temperature Protection (Thermal Shut Down))	PN Junction temperature	

1.UVLO(Under Voltage Lock Out)

If VIN voltage is 7.3V or lower, then UVLO operates and the IC stops. When UVLO operates, the power supply current of the IC is about 80uA or lower. If VIN voltage is 9V or higher, then the IC starts switching operation.

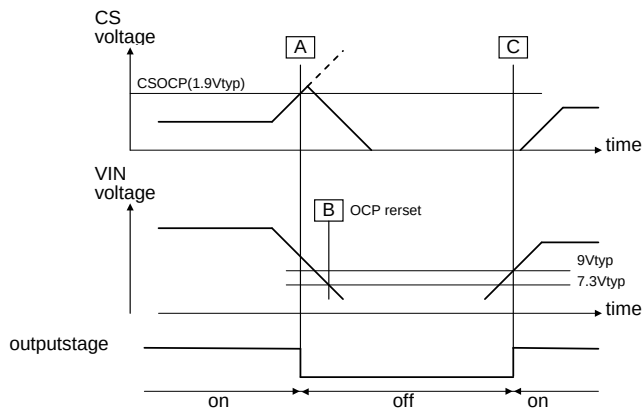


2.OC(Over Current Protection)

The CS pin sense the current through the MOS FET switch and the primary side of the transformer.This provides an additional level of protection in the event of a fault. If the voltage of the CS pin exceeds VCSOCP(1.9Vtyp)(A), the internal comparator will detect the event and turn off the MOSFET. The peak switch current is calculated

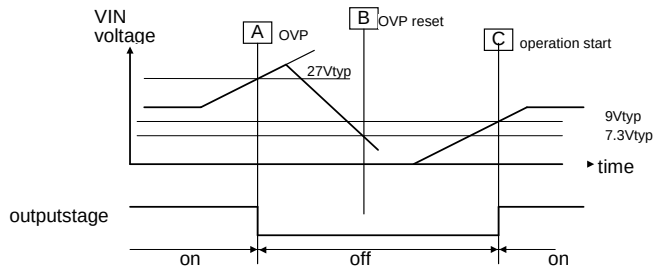
$$I_{o(peak)} [A] = V_{SOCP}[V]/R_{sense}[ohm]$$

The VIN pin is pulled down to fixed level, keeping the controller latched off.The lach reset occurs when the user disconnects LED from VAC and lets the VIN falls below the VIN reset voltage,UVLOFF(7.3Vtyp)(B). Then VIN rise UVLOON(9Vtyp)(C),restart the switching.



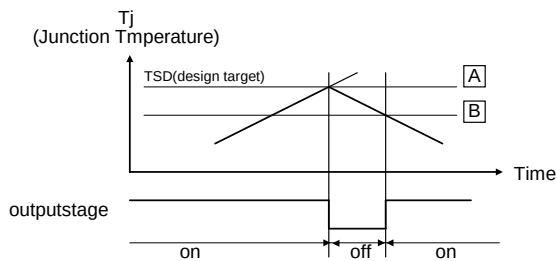
3.OVP(Over Voltage Protection)

If the voltage of VIN pin is higher than the internal reference voltage VINOVP(27Vtyp),switching operation is stopped. The stopping operation is kept until the voltage of VIN is lower than 7.3V. If the voltage of VIN pin is higher than 9V, the switching operation is restated.



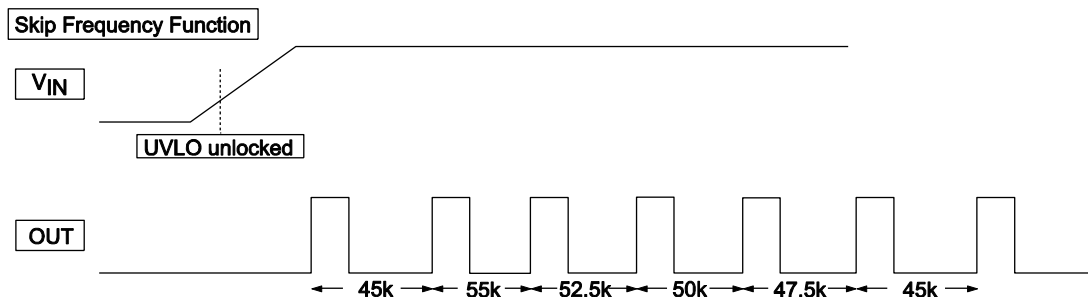
4.TSD(thermal Shut Down protection)

The thermal shutdown function works when the junction temperature of IC is 165°C (typ) (A), and the IC switching stops. The IC starts switching operation again when the junction temperature is 135°Ctyp (B) or lower.



Skip frequency function

LV5027M contains the skip frequency function for reduction of the peak value of conduction noise. This function changes the frequency as follows.



Switching frequency is changed as follows.
 $\dots \times 0.9 \rightarrow \times 1.1 \rightarrow \times 1.05 \rightarrow \times 1 \rightarrow \times 0.95 \rightarrow \times 0.9 \rightarrow \times 1.1 \dots$
 It's repeated by this loop.

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